

Errata for the Dally/Poulton "Digital Systems Engineering" Text.

This list compiled by Fred Rosenberger (fred@cse.wustl.edu, <http://www.cse.wustl.edu/~fred>) as an aid to anyone using the Dally/Poulton text. I expect some of the "errors" reported here are misunderstandings or misconceptions on the part of myself or the person reporting them so use with caution. Additions and corrections to this list welcomed.

First: This is a very good text/reference. Lots of highly relevant material, broad coverage, authoritative. I have used it in CoE464 because I believe it is the best available text.

| PAGE | Cm from Page Top | Original Text | Reported By | Date (Warning, not Y2K compliant) | |
|------|---------------------------|--|---|--|-----------|
| 52 | Table 2-3 | | RG-178B/U and M17/133 have the same impedance and velocity but different pf/m. Not possible. | FUR | Jan-6-99 |
| 83 | Eq 3-7 | d | should be s to correspond to Figure 3-2(e) | E464 Class Spring 1999 | Jan-30-99 |
| 84 | Table 3-2 | | Values in this table differ from those on inside front cover by more than just rounding | FUR | Jan-6-99 |
| 93 | Eq 3-32, 3-36, ... | 3-32 has $I_r = V_r/Z_o$ but later is $I_r = -V_r/Z_o$ | Either can be correct depending on the definition of I_r but it should be consistent. The first form goes with I_r being defined as positive for current from right to left. | FUR | Jan-23-99 |
| 95 | Fig 3-8 | Has V_i and I_f | Not consistent. Seems both subscripts should be i (incident) or f (forward) Same for other equations. Also seems that either i or f should be used throughout, not a mixture (unless there is hidden distinction that I miss). | FUR | Jan-23-99 |
| 104 | last line | "a 5-mil copper stripguide" | Is this stripline or microstrip? 0.5oz or 1oz, width, spacing, ...? Stripguide is not in the index and I am not sure what geometry is meant here | FUR | Mar-12-99 |
| 105 | Fig 3-19 | 30 AWG Pair (two places) | 24 AWG Pair | FUR | Jan-23-99 |
| 271 | | 1. Wiring ground rules ... | <- Wiring rules ... ground rules in the original has two interesting meanings, ground as in 0 potential, and ground rules as in baseball. I spent time figuring out which was intended and the word ground really adds nothing here. | FUR | Mar-12-99 |
| 276 | Tbl 6-3 | | Please give units (C, L, ...) in table, not just in text. Also please give meaning of asterisk in table, not just text | FUR | Mar-12-99 |
| 276 | 3rd last line | "all dimensions are in mils" | This only matters if the conductors have specific thickness, otherwise only ratios matter and units could be anything. Line thickness is not given, is it 0.5 oz? | FUR | Mar-12-99 |
| 276 | Tbl 6-3 | C and Cm | On page 110 capacitance is specified in Cs and Cc | FUR | Mar-12-99 |
| 277 | | 15.8 "are grounded at one end" | This depends on the type of coupling but I believe for high speed digital signals this should be "are grounded at both ends" assuming the shield has its ends close to the ends of the shielded wires. | FUR | Jan-30-99 |
| 279 | Fig 6-15 | | R2 cannot change when A1 does, this would be 0 prop delay. Direction of change also is suspect. Finally, it's the voltage across the termination resistors that matters and this is not calculated or shown. This really should be analyzed from the viewpoint of coupled lines | FUR | Mar-12-99 |
| 298 | 3rd line before 6.7 | "made on a statistically significant sample of channels ..." | Seems covering the range of allowed fab parameters is more important than number of samples. Noise components such as offsets are not random, and there is no number of samples that is gaurenteed to reasonably cover the range without more info | FUR | Mar-12-99 |

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|-------------------|---|---|---|----------------------------------|------------|
| 308 | Section 7.1.1: Calculation of PD for CMOS case may be misleading. | With 50% duty cycle, max PD with 200 Ohm output R is: $0.5 \cdot V^2 / R = 0.5 \cdot 3.3^2 / 200 = 27\text{mW}$, much less than the 130mW given in 7.1.1. This is partially due to the fact that the circuit can't switch at 100MHz. Of course limitation to less than 100 MHz is a big disadvantage. Output R could be set to 50 Ohms with wider FETs, this would allow operation at 100MHz and would increase max PD to 108mW. This 108mW is still a little still less than the 130mW calculated in 7.1.1 because the round trip delay of the example is 12ns, longer than the period between data changes. Once the round trip delay is longer than the period between data changes, no additional power is required to increase the data rate. Note that if data value changes infrequently PD for the full-swing CMOS can actually be lower than LSC case. Random data would have a transition every other cycle on the average and PD of 54mW. | FUR | Jan-7-99 | |
| 309 | Tbl 7-3 | From page 307, offset is +/-10mV and sensitivity is 10mV. This should give Vih and Vil of +/-15mV. | FUR | Mar-12-99 | |
| 311 | 2nd line before 7.1.3 | "because most CMOS drivers do not ..." | But they could. Does not seem fair to give advantage to LSC here because CMOS could do this also. | FUR | Mar-12-99 |
| 312 | 2nd line 7.1.4 | "Yet it is far from optimal in almost any application" | It is optimal in number (or area) of components | FUR | Mar-12-99 |
| 318 | Fig 7-7 | | Both parts of the Figure are labeled (a) | FUR | Mar-12-99 |
| 319 | Fig 7-8 | | Ir could be reduced for unipolar signaling to improve its performance. The two schemes would then be about equal (with illustrated values). | FUR | Mar-12-99 |
| 323 | Fig 7-13 | | This might be drawn closer to the form in Fig 7-4 to make correlation between the Figures easier. | FUR | Mar-12-99 |
| 329 | 4th line from bottom | | In some ECL based CRAY computers, unused outputs (ECL has two complementary outputs) were terminated just to keep the current approximately constant when switching | FUR | Mar-12-99 |
| 331 | 2nd line | "it is better to model ..." | Seems its <i>easier</i> to model as lumped circuit, but more accurate to model as distributed. | FUR | Mar-12-99 |
| 349 | Fig 7-41 | | Is Vrs consistently defined in the text. Seems somewhere its defined as half that in Fig 7-41? | FUR | Mar-12-99 |
| 510 | 19.8 | Rosenburger | Rosenburger | FUR | Feb-15-99 |
| 648 | 15.7 | Rosenburger | Rosenburger | FUR | Jan-6-99 |
| 659 | 21.1 | Stackup, 44 | Stackup, 41 | FUR | Jan-6-99 |
| Inside back cover | | | Equation for wire over ground plane capacitance needs 2 added in numerator. Equation for Zo needs 2 added in denominator. | FUR | Feb-06-99 |
| 388 | Fig 8-32 | Legend to right of middle plots refers to solid and dashed but both traces are solid | | Dan Lenoski, Growthnetworks Inc. | Mar-26-99 |
| 437 | Fig 9-38 | | Clock adjust block should show clock input | FUR | Apr-3-1999 |
| 440 | Fig 9-42 | | Clock adjust block should show clock input | FUR | Apr-3-1999 |
| 469 | 2nd Par in 10.2.2.2 | | Dealing with noise its necessary to consider an ensemble of events, not a single isolated event. I don't understand the last sentence. It can be shown that including noise for ensemble of events gives approximately same result as noise free case | FUR | Apr-3-1999 |
| 469 | 3rd Par in 10.2.2.3 | "The value of delV1 is uniformly distributed between 0 and 1" | This is a safe bound on the initial voltage (but should be -Vdd and Vdd, not 0 and 1) but is very conservative. | FUR | Apr-3-1999 |
| 470 | Table 10-1 | | Does not give tau_s | FUR | Apr-3-1999 |

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|----------------------------------|--|--|----------------|-------------|
| 470 line 11 | "one clock period less t_{dCQ} , t_w approx 10ns | A Figure is needed for at latch (or flop) showing the definition of t_w . When does this period start? At clock edge, or t_{dCQ} after clock edge? Also, setup time should be subtracted from clock period since valid value is required at second flop input a setup time before clock | FUR | Apr-3-1999 |
| 471 5th line from bottom | τ_r | should be τ_s | FUR | Apr-3-1999 |
| 472 2nd Par | | Reference Flannagan (JSSC Aug 85, pp880-882, sc-20, no 4) which shows optimum τ_s is obtained with equal width N- and P-FETS. | FUR | Apr-3-1999 |
| 477 13th line from bottom | "places the keep-out region into the receiver's" | Sentence is garbled. | FUR | Apr-3-1999 |
| 104 last line | "5-mil copper stripguide" | w and h are given but not s. Is this 50 Ohm impedance? Configuration? | FUR | Apr-3-1999 |
| 226 first line | | change "drops" to drop | FUR | Apr-16-1999 |
| 232 6th line | | change "increase" to "decrease" | FUR | Apr-16-1999 |
| 405 line 2 | | Change "BC" to "AC" | EE464 De Alwis | Apr-16-1999 |
| 418 Sec 9.5.2, next to last line | | "Two-Phase clocking is the most common ..." In what context? Not at PC board level. Not in edge-triggered ASIC design. Not in FPGAs. Unless we look inside flops at their internal structure. | EE464 De Alwis | Apr-16-1999 |
| 369 Fig 8.16, Eq 8-9 | | I_b is used twice, once for the bias current sources (in figure), once for the difference output current (ΔI_b in Eq 809) | EE464 De Alwis | Apr-16-1999 |
| 326 Eq 7-15 and 7-16 | | both lower case and upper case B is used in subscripts but it seems they should all be the same. | EE464 De Alwis | Apr-16-1999 |
| 329 13.2cm | "twice the noise margin" | Should be more than twice the noise margin if drive is doubled and receiver sensitivity stays the same. | EE464 De Alwis | Apr-19-1999 |
| 329 14.2cm | "rise- or fall-time affecting ... half the transistion time" | This could be stated more clearly: dv/dt is twice ... | EE464 De Alwis | Apr-19-1999 |
| 511 Prob 10-1 | | τ_r should be τ_s . Why is t_{dCQ} included (see comments about page 470)? t_a is not given (could be determined if rise time were given) | EE464 Hussain | Apr-19-1999 |
| 307 line 7 | | 2x3.3mA/50Ohm should be 2X3.3mAx50Ohm | EE464 Hussain | Apr-19-1999 |
| 468 second line after Eq 10-1 | $K_s = I/C$ approx $1/t_a$ | Where does this come from? It at least needs a reference or an explanation. This is approximately the value for any delay (t_{dCQ} , t_s , t_h , ...) | FUR | Apr-19-1999 |
| 469 Eq 10-3 | | $\log(\Delta V_1)$ does not have correct units. Should be $\log(\Delta V_1/1V)$. Although the actual value of voltage used (1V in this case) is not very important in overall reliability calculations, carrying it along in the calculations makes the understanding and checking much easier. | FUR | Apr-19-1999 |
| Chapt 12 | | Chapter 12 on timing circuits could include a section on design of (and analysis of) flip-flop metastability parameters. How to design flops for good resolving time. Use Flanigan (sp?) ref and others. | FUR | Apr-19-1999 |
| 399 line 3 | | "loop has low bandwidth, it is unable to track and cancel the high-frequency jitter." If clock to clock jitter is independent then there is no loop bandwidth that would cancel jitter. | FUR | Apr-19-1999 |
| 399 Eq 9-1 | | This equation should include t_{dCQ} . Clearly t_{dCQ} has the same effect as wire delay in series with the transmit flop output so it must be part of the equation. | FUR | Apr-19-1999 |

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| 363 line 7 | | Figure 8-8 should be Figure 8-7 | EE464 Hussain | Apr-19-1999 |
| 460 Prob 9-7 | | "Table 9-7" should be Table 9-9. Table 9-9 at top of page should refer to problem 9-7, not Figure 9-7. | FUR | Apr-19-1999 |
| back cover | | k _r in reflection coefficient is lower case k, but in Eq 3-38 reflection coefficient is upper case K (but lower case in Eq 3-37) | FUR | Apr-19-1999 |
| 482 Fig 10-17 | | This seems to have a synchronization problem in the flops just after t _m . If the value of xp is changing from 010 to 001, then sdxp might be: 000, 010, 011, or 001. Two of these are ok, two are not and must be detected and dealt with. | FUR | Apr-19-1999 |
| Genera l | | A glossary of terms, and more importantly symbols, would be a great help to the reader. Also it would help eliminate multiple symbols for the same parameter (k vs K for reflection coefficient, tau _r vs tau _s for metastability time constant, ...) | FUR | Apr-19-1999 |
| 308 5th line from bottom | "noise immunity" | What is definition of noise immunity? | FUR | Apr-26-1999 |
| 398 Fig 9-2 | "RxClk-to rest of receive chip" | Why take from indicated position? Phase is unknown with respect to data flop clock. | FUR | Apr-26-1999 |
| 407 Eq 9-13 | | Reverse -t _{ao} and +t _{ao} in first two lines | De Alwis | Apr-26-1999 |
| 95 below eq 3-36 | "Telegrapher's equation" | Poon and others call eq 3-26 the telegrapher's equation. Matick does not refer to it. I think common usage is that eq 3-26 is the telegraphers equation, not 3-36 | FUR | May-08-1999 |
| 364 8.2.2 caption | "Equalization ... " | "equalization" is not in the index | FUR | May-08-1999 |
| 469 line 2 | "to attain unit voltage" | I realize that it makes little (actually no) practical difference, but the use of unit voltage here causes the units to get lost (e.g. units in eq 10-3 don't balance as you can't take the log of Volts. It would become ln(delta_V1/Vdd)). Use of Vdd, rather than unit voltage has a lot of pedagogical advantages including units, scaling to different voltages, etc. | FUR | May-08-1999 |
| 469 eq 10-3 | | Use of log for log_base_e is mildly confusing sometimes (I think this happens other places in text also). Many texts use ln for log_base_e and log for log_base_10. Seems a little safer and conventional. | FUR | May-08-1999 |
| 319 Par. 2 | "Bipolar signalling reduces power ..." | Peak current is 1/2, but current is required 100% of the time rather than 50% so total power is the same | FUR | Mar-01-2000 |
| 469 7th line from bottom | "uniformly distributed between 0 and 1" | This needs significantly more justification and rationalization. | FUR | Mar-14-2000 |
| 582 next to last par | "edge-triggered flip-flop" | latch | FUR | Mar-14-2000 |
| 122 Fig 3-32 | | Explicit representation for ground(s) would help here | FUR | Mar-14-2000 |
| 297 Line 123 | "gross noise margin" | In text gross noise margin is delta-V/2 - V _N . In Lecture notes 6, slide 14, gross margin is delta-V/2, are these supposed to be the same or are we to have two gross margins (one with "noise" as part of name)? | De Alwis | April-26-2000 |
| 470 10.2.2.4, second last line | 2.59*10 ⁻¹⁷ | 2.59*10 ⁻¹⁷ | Scott Moran | April-08-2001 |
| 407 line 4 | t _{dDQ} | t _{dCQ} | Karen Ng | April-04-2002 |

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|-------------------------|------------------------------|--|---------------------|---------------|
| 437 Fig 9-38 | | I don't think this phase comparator works as shown. Would give 1/2 Vdd as filtered value. Text at end of paragraph says 9-38 is identical to 9-2, but 9-2 has two flops and an ex-or for the phase comparator. | FUR | April-09-2003 |
| 83 Eq 3-7 | we/s | w eps/s (error created in fixing earlier error) | Teddy Lee | Feb-4-2003 |
| Inside Back cover | microstri p formula | C should be: $\text{eps} * w / s + 2 * \pi * \text{eps} / (\ln(2 * s / h / 2))$ | FUR | Feb-4-2004 |
| Inside Back cover | wire over ground plane | For Zo, the pi in the denominator should be 2*pi | FUR | Feb-4-2004 |
| Inside Back cover | | In equation for parallel plate characteristic impedance, the W should w (lower case) to correspond to the Figure | FUR | Feb-4-2004 |
| 106 Eq 3-56 | | $\text{epsilon}_k < \text{epsilon}_r$ | Joseph Lancaster | Mar-2-2004 |